

Bode optimal loop shaping with CRONE compensators

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14th IEEE Mediterranean Electrotechnical Conference
5-7 May 2008, Ajaccio, France

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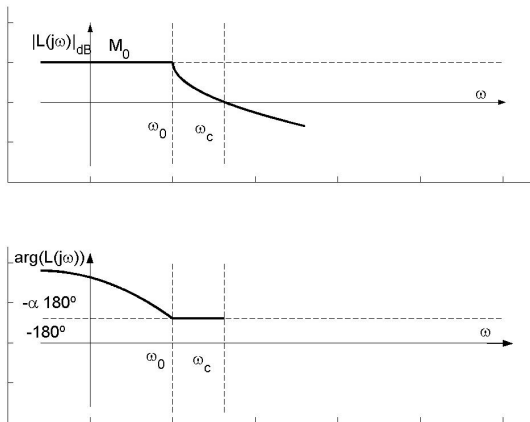
Problem Statement

- PROBLEM:
 - for operational bandwidth $0 \leq \omega \leq \omega_0$
 - where desired $|L(j\omega)| = M_0 \gg 1$
 - given crossover frequency ω_c
 - compute $L(j\omega)$ which maximizes ω_0
- SOLUTION: decrease $|L(j\omega)|$ as fast as possible...

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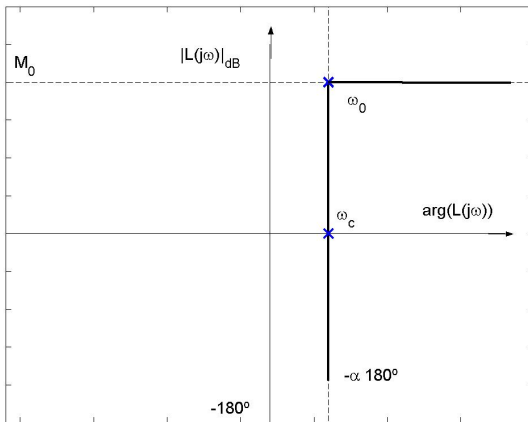
Ideal Bode Characteristic

For ideal optimal structure $\begin{cases} |L(j\omega)| = M_0, & 0 < \omega < \omega_0 \\ \angle L(j\omega) = -\alpha\pi, & \omega > \omega_0 \end{cases}$

solution is equivalent to maximize phase lag,
or minimizing stability margin,
so it is necessary to trade-off between ω_0 and stability margin...

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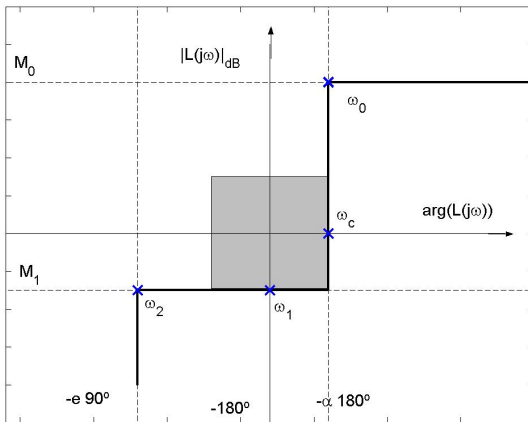
Four Parameters Bode Optimal Loop

- In general, the problem is well defined as a function of parameters:
 - M_0
 - α
 - ω_0
 - ω_c
- Not all of them independent.

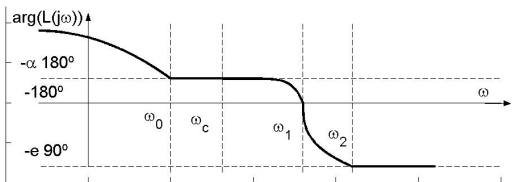
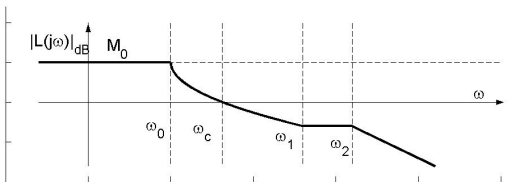
Practical considerations about high frequency

- In practice, four parameters Bode Optimal Loop has to be modified:
 - To cope with sensor noise amplification
 - Because it is not realistic to assume good control of $|L(j\omega)|$ for high frequency.

Seven Parameters Bode Optimal Loop



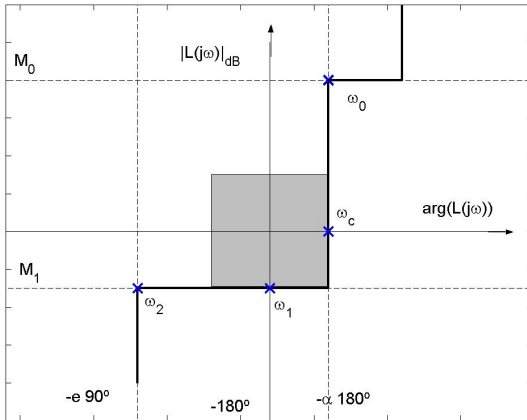
Seven Parameters Bode Optimal Loop



Eight Parameters Bode Optimal Loop

In order to add integrators to the loop, for a good steady state response ...

Eight Parameters Bode Optimal Loop



Eight Parameters Bode Optimal Loop

- Parameters:
 - M_0
 - M_1
 - α
 - ω_0
 - ω_c
 - ω_1
 - n
 - e
- Not all of them are independent.

Our Goal

Establish **relations between** these **eight parameters** and the **parameters of** a proposed **CRONE structure**, so that a first approach to Bode optimal loop can be obtained in an easy and fast way.

CRONE Features for Bode Optimal Loop Shaping

- Easy to tune
- Few parameters
- For the 2/3 CRONE generation band defined compensator

$$D_r = \left(C_0 \frac{1 + \frac{s}{\omega_l}}{1 + \frac{s}{\omega_h}} \right)^a \cos \left[-b \operatorname{Log} \left(C_0 \frac{1 + \frac{s}{\omega_l}}{1 + \frac{s}{\omega_h}} \right) \right],$$

- Phase and gain slope only depend on a (real differentiation order)
- Gain and phase slope only depend on b (complex differentiation order)
- Idea: for a Bode optimal loop shape, with constant phase at (ω_l, ω_h) and constant gain at (ω'_l, ω'_h) , use real differentiator at (ω_l, ω_h) ($b=0$) and complex differentiator ($a=0$) at (ω'_l, ω'_h) .

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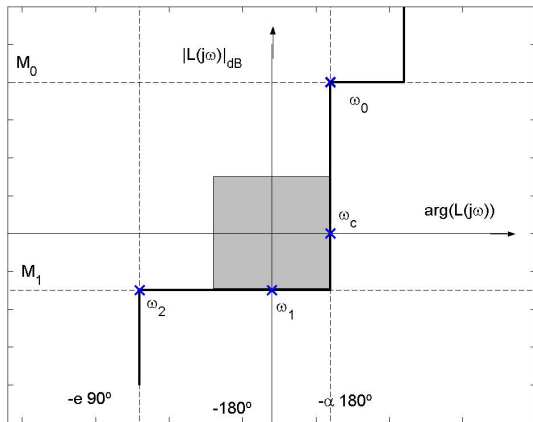
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CRONE Features for Bode Optimal Loop Shaping

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- For the 2/3 C
 - $D_r = \left(C_0 \frac{1+s}{1+s/c} \right)$
 - Phase an order
 - Gain and differentia
- Idea: for a Bc at (ω_l, ω_h) an differentiator $(a=0)$ at (ω'_l, ω'_h)



CRONE Features for Bode Optimal Loop Shaping

- Additionally, two terms to shape low and high frequencies
- Final structure:

$$L(s) = k \left(\frac{\omega_l}{s} + 1 \right)^{n_l} \left(C_0 \frac{1 + \frac{s}{\omega_l}}{1 + \frac{s}{\omega_h}} \right)^a$$
$$\cos \left[-b \operatorname{Log} \left(C'_0 \frac{1 + \frac{s}{\omega'_l}}{1 + \frac{s}{\omega'_h}} \right) \right] \frac{1}{\left(\frac{s}{\omega_h} + 1 \right)^{n_h}}$$

Real Differentiator Term

- $L_2(s) = \left(C_0 \frac{1 + \frac{s}{\omega_l}}{1 + \frac{s}{\omega_h}} \right)^a$
- Design relations:
 - $a \left(\frac{\pi}{2} - 2\theta_l(\omega_u) \right) = (1 - \alpha)\pi$
 - $\left(\frac{\omega_h}{2\omega_l} \right)^{-a} \approx M_0 M_1$

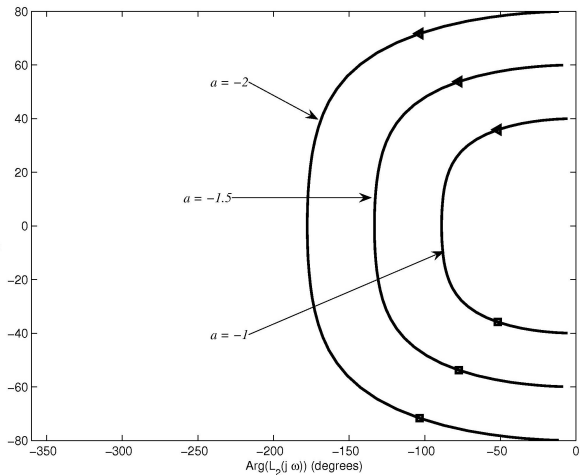
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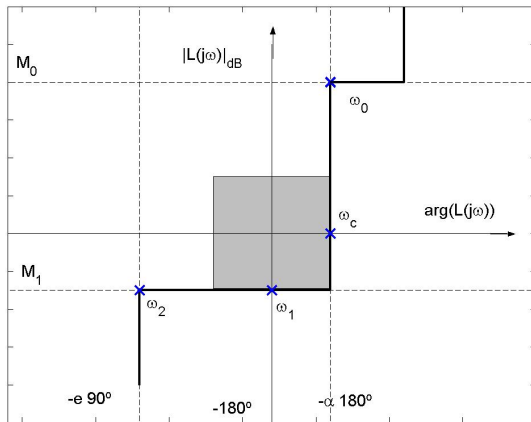


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Low and High Frequency Terms

- $L_{CRONE2}(s) = k \left(\frac{\omega_l}{s} + 1 \right)^{n_l} \left(C_0 \frac{1 + \frac{s}{\omega_l}}{1 + \frac{s}{\omega_h}} \right)^a \frac{1}{\left(\frac{s}{\omega_h} + 1 \right)^{n_h}}$
- Design relations:
 - $n_l \geq n$
 - $n_h \geq e_p \geq n$
 - $|L_{CRONE2}(j\omega_c)| = 1$
 - $|L_{CRONE2}(j\omega_u)| = \frac{M_{0,dB} + M_{1,dB}}{2}$

Low and High Frequency Terms

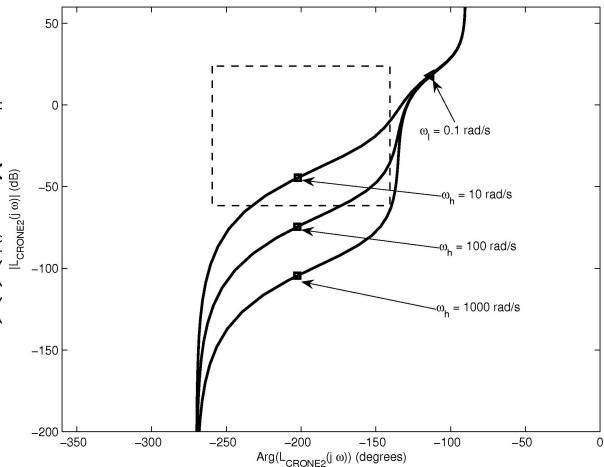
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Complex Differentiator Term

- $L_3(s) = \cos \left[-b \operatorname{Log} \left(C'_0 \frac{1 + \frac{s}{\omega'_l}}{1 + \frac{s}{\omega'_h}} \right) \right]$
- Complements $L_2(s)$, to increase phase lag at $[\omega'_l, \omega'_h]$
- To avoid non minimum phase:

$$b \log \left(\frac{\omega'_h}{\omega'_l} \right) < \pi$$

or, equivalently

$$b < b_{max} = \frac{\pi}{\log(\omega'_h/\omega'_l)}$$

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Maximizing Loop Phase Lag

- Maximized by $b = b_{max}$, but...
- Design relations:
 - $\omega'_U = \omega_h \approx \omega_1$
 - $b \approx b_{max}$

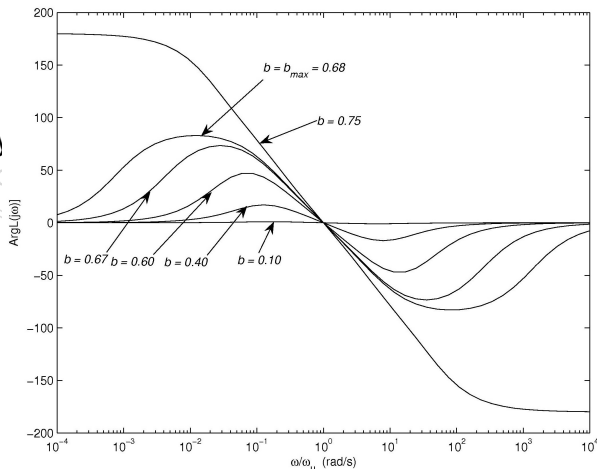
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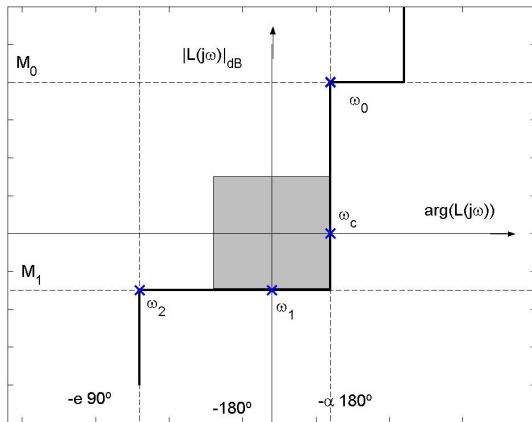


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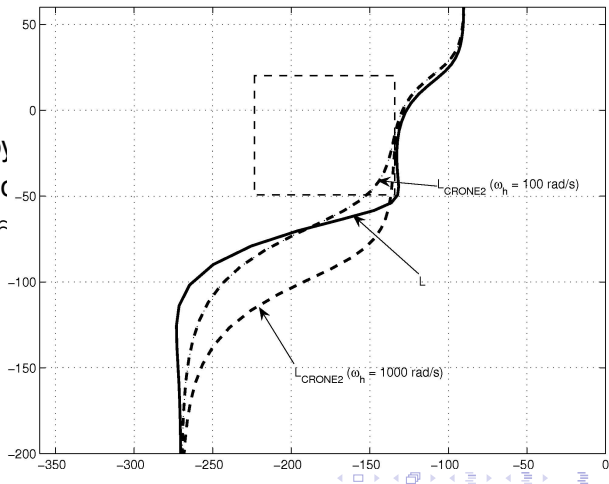
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Desig Example

- 8 Parameters Bode Optimal Specifications:
 - $M_{0,dB}=M_{1,dB}=30$ dB
 - $\omega_0 = 0.4$ rad/s, $\omega_c = 0.4$ rad/s
 - $\alpha = 0.22$ (40° phase margin)
 - $e = 3$, $n = 2$
 - $\omega_1 = 40$ rad/s
- Loop obtained:

$$L_{ex}(s) = 0.87 \left(\frac{0.34}{s} + 1 \right)^2 \left(C_0 \frac{1 + \frac{s}{0.34}}{1 + \frac{s}{93.5}} \right)^{-1.45} \cos \left[-1.8374 \operatorname{Log} \left(C'_0 \frac{1 + \frac{s}{97.5}}{1 + \frac{s}{250}} \right) \right] \frac{1}{\left(\frac{s}{93.5} + 1 \right)^3}$$

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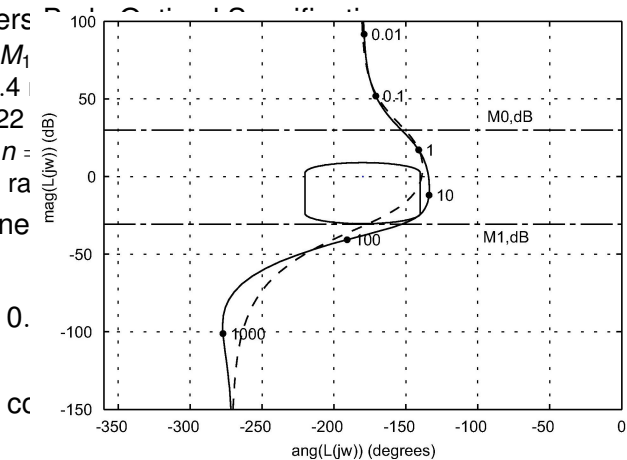
Design Example

- 8 Parameters

- $M_{0,dB} = M_1$
- $\omega_0 = 0.4$
- $\alpha = 0.22$
- $e = 3, n = 1$
- $\omega_1 = 40$ rad/s

- Loop obtained

$$L_{ex}(s) = 0.$$



Conclusions

- A special CRONE compensator has been proposed to efficiently approximate Bode optimal loop.
- Bode optimal loop has been defined based on a number of parameters, and simple design rules have been obtained for tuning the proposed compensator.
- These rules yield a first solution of a rather hard problem.
- A finest tuning may require the use of some automatic loop shaping technique.

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